











## Article

# An Integrated Geophysical Approach to Characterise the Behaviour of a Fault Zone in Relation to Fluid Migration During CO<sub>2</sub> Geological Storage: The Case of the Matzaccara Fault in the Sulcis Coal Basin (Sardinia)

Valentina Volpi <sup>1,\*</sup>, Cinzia Bellezza <sup>1</sup>, Dario Civile <sup>1</sup>, Flavio Accaino <sup>1</sup>, Erika Barison <sup>1</sup>, Piero Corubolo <sup>1</sup>,  
Biancamaria Farina <sup>1</sup>, Edy Forlin <sup>1</sup>, Massimo Giorgi <sup>1</sup>, Michela Giustiniani <sup>1</sup>, Fabio Meneghini <sup>1</sup>,  
Alberto Pettinau <sup>2</sup>, Alberto Plaisant <sup>2</sup>, Andrea Schleifer <sup>1</sup> and Flavio Poletto <sup>1</sup>

<sup>1</sup> National Institute of Oceanography and Applied Geophysics-OGS, Sgonico, 34010 Trieste, TS, Italy; cbellezza@ogs.it (C.B.); dcivile@ogs.it (D.C.); faccaino@ogs.it (F.A.); ebarison@ogs.it (E.B.); pcorubolo@ogs.it (P.C.); bfarina@ogs.it (B.F.); eforlin@ogs.it (E.F.); mgiorgi@ogs.it (M.G.); mgiustiniani@ogs.it (M.G.); fmeneghini@ogs.it (F.M.); aschleifer@ogs.it (A.S.); fpoletto@ogs.it (F.P.)

<sup>2</sup> Sotacarbo S.p.A., Grande Miniera di Serbariu, 09013 Carbonia, CA, Italy; alberto.pettinau@sotacarbo.it (A.P.); albertoplai@tiscali.it (A.P.)

\* Correspondence: vvolpi@ogs.it

## Abstract

In February 2024, the European Union published its Industrial Carbon Management Strategy, setting ambitious goals for carbon capture and storage (CCS), carbon capture and utilisation (CCU), and related technologies. Industrial decarbonisation will require a mix of solutions, CCUS, electrification, hydrogen and hydrogen-derived fuels, and energy efficiency, which are all dependent on affordable clean energy. Although carbon management technologies could contribute substantially to climate targets, their deployment has been slowed by technical barriers and public concerns. Sotacarbo has created a research centre dedicated to developing and testing carbon capture, utilisation, and storage technologies. Within this framework, the new Sotacarbo Fault Laboratory (SFL) was designed to investigate gas migration in faults and to test monitoring systems capable of detecting potential short- and long-term CO<sub>2</sub> leakages. This paper presents a preliminary study, including seismic full-waveform simulations for time-lapse surveys before and after CO<sub>2</sub> injection, and a suite of geophysical methods used to characterise the Matzaccara Fault within the Eocene Sulcis Basin. The results of the application of integrated geophysical methods support the selection of a safe and suitable injection-well location and demonstrate the value of these methods for detailed fault characterisation in CCUS applications.

**Keywords:** carbon capture, utilisation, and storage (CCUS); fault zone characterisation; CO<sub>2</sub> monitoring and leakage detection; multichannel seismics; borehole geophysics



Academic Editor: Meng Lu

Received: 22 December 2025

Revised: 25 January 2026

Accepted: 27 January 2026

Published: 2 February 2026

**Copyright:** © 2026 by the authors.

Licensee MDPI, Basel, Switzerland.

This article is an open access article distributed under the terms and

conditions of the [Creative Commons](https://creativecommons.org/licenses/by/4.0/)

[Attribution \(CC BY\)](https://creativecommons.org/licenses/by/4.0/) license.

## 1. Introduction

The European Union's strategy to combat global warming caused by the ongoing emission of greenhouse gases assigns carbon capture, utilisation, and storage (CCUS) a crucial role in the EU Green Deal for the transition of energy-intensive industries and the power sector [1]. It is therefore essential to develop CCUS for industrial clusters, including system planning and shared infrastructure solutions [2]. This can be achieved by demonstrating the full CCUS chain in the EU, focusing on reducing energy losses

and capture costs, and implementing solutions for geological storage, both onshore and offshore [3]. Onshore storage will support the management of decarbonisation strategies at the territorial level, while improving energy security, local economic activities, and safeguarding jobs across Europe [4,5]. However, successful onshore storage also requires addressing specific technical and societal challenges including development, testing, and demonstration of key technologies specifically adapted for onshore storage under real-world conditions, contributing to the creation of a favourable environment for onshore storage across Europe through public acceptance. To support progress in geoscientific research and meet the global demand for safe, sustainable, and secure CO<sub>2</sub> storage sites, both onshore and offshore, these challenges need to be thoroughly characterised and monitored to reassure the public and comply with EU legislation [6]. Methodologies and procedures should be developed to detect, attribute, and quantify any leakage from a CO<sub>2</sub> storage complex to the surface and into the environment. Research, innovation, testing, and verification require research infrastructures and services to address major challenges such as testing and engineering materials, drilling technologies, modelling and assessment of geomechanics and induced seismicity, and reservoir evaluation and management. Environmental monitoring technologies are also becoming increasingly important as the focus shifts from technical development to pilot projects, demonstrations, and real-world deployment of low-carbon geoenergies [7].

In this context, Sotacarbo, a research and development company (with shareholders that include the Regional Government of Sardinia and ENEA, the Italian National Agency for New Technologies, Energy and Sustainable Economic Development) located in the south-western corner of Sardinia (Italy), in collaboration with the Universities of Cagliari and Rome “La Sapienza”, OGS (National Institute of Oceanography and Applied Geophysics), INGV (National Institute of Geophysics and Volcanology), and RSE (Research on Energy Systems), has launched an ambitious research programme funded by the Italian and Sardinian regional governments to explore the Sulcis coal basin as a potential site for testing technologies for CO<sub>2</sub> geological storage [8,9]. This includes methods for capturing carbon dioxide emissions from industrial processes and power generation plants (including biomass gasification systems), as well as research into ways of storing or utilising captured CO<sub>2</sub>. For this reason, Sotacarbo’s facilities are integrated into the ECCSEL ERIC network (European Research Infrastructure for CO<sub>2</sub> Capture, Utilisation, Transport and Storage), which has covered the entire CCUS chain since its foundation. In particular, the Sotacarbo Fault Laboratory (SFL) facility has been designed specifically to study gas migration processes across faults and to test a wide range of monitoring technologies that are fundamental for detecting potential short- and long-term unwanted CO<sub>2</sub> leakages.

Various regional-scale studies on CCS (Carbon Capture and Storage) have been published in Italy to date, mostly focusing on identifying areas potentially suitable for CO<sub>2</sub> storage in saline aquifers [10–13]. This work presents a local case study analysed in detail, focusing on the Matzaccara normal fault in the south-western part of the Sulcis coal basin, which was identified and selected as the target tectonic structure for the SFL research activities. The Matzaccara Fault was chosen as a test site because it exhibits the most recent tectonic activity among the faults identified in the southern Sulcis Basin and presents a near-surface fault plane.

This paper presents a detailed local-scale case study of the Matzaccara normal fault in the Sulcis coal basin, selected as a test site for CO<sub>2</sub> storage research. This study integrates high-resolution seismic reflection data, borehole stratigraphic information, and downhole geophysical measurements (including VSP and geoelectrical data) to characterise the fault geometry and identify an optimal location for a CO<sub>2</sub> injection well. In addition, this work

evaluates the effectiveness of integrated geophysical monitoring techniques for assessing subsurface conditions and well integrity before, during, and after CO<sub>2</sub> injection.

The aim of this work is to apply a multidisciplinary workflow for the high-resolution geophysical characterisation of a test site to investigate the behaviour of CO<sub>2</sub> injected at a shallow fault. This study also demonstrates the feasibility of geophysical monitoring in a volcanic context with a weak seismic response, defines operational criteria for well design and data acquisition parameters, and provides an experimental framework to test advanced monitoring techniques in a CCS fault-controlled scenario. The role of geophysics in carbon capture, utilisation, and storage (CCUS) applications is vital. These methods are essential for ensuring the safe and effective containment of CO<sub>2</sub> and the long-term sustainability of storage sites, thereby underpinning the success and reliability of CCUS initiatives.

## 2. Geology of the Sulcis Coal Basin

The Sulcis coal basin covers an onshore-offshore area of approximately 800 km<sup>2</sup> and its basement consists of Palaeozoic metamorphic rocks and large volumes of granitoids related to the Hercynian Orogeny [14], locally overlain by Permo-Carboniferous terrigenous and volcanic complexes. Above these, there lies a predominantly Mesozoic carbonate succession of platform and basin environments [15]. This is followed by a Palaeogene transgressive–regressive sedimentary cycle [16–19] consisting of a 30–60 m thick carbonate succession assigned to the Early Eocene Miliolitico Formation, composed of shallow-water fractured limestones rich in macroforaminifera, evolving into wackestone and mudstone with an ologotypical miliolid fauna [20]. The Miliolitico Formation has been proposed as the main reservoir for CO<sub>2</sub> injection [9,21]. A rhythmic succession of siliciclastic to carbonate deposits up to 100 m thick contains lignite intercalations and is attributed to the Early Eocene Produttivo Formation [22]. A Middle Eocene–Oligocene continental alluvial succession up to several hundred metres thick is also present, known as the Cixerri Formation [16,23–25]. The uppermost part of the Sulcis basin succession consists of more than 900 m of Lower to Middle Miocene volcanic rocks, ranging from basaltic to rhyolitic composition [26–28]. In the southern sector of the basin, the lower part of the volcanic sequence, which consists of andesites and basalts, is absent. The volcanic rocks are locally overlain by marine, lacustrine, alluvial, and aeolian unconsolidated Quaternary sediments [20,29].

The study area is located in the southern sector of the Sulcis coal basin (see location Figure 1a and stratigraphy in Figure 1b), where Sotacarbo has been granted a research permit for CCS-related studies. This area is affected by E–W, N–S, and NE–SW high-angle normal faults formed during Miocene extensional phases [10,22]. The main structure is the NNE-oriented Matzaccara Fault (Figure 1a). The northern part of this structure was analysed using three high-resolution seismic profiles (Figure 1a) to assess whether it could be a suitable target for studying fault behaviour in relation to fluid migration resulting from CO<sub>2</sub> injection.

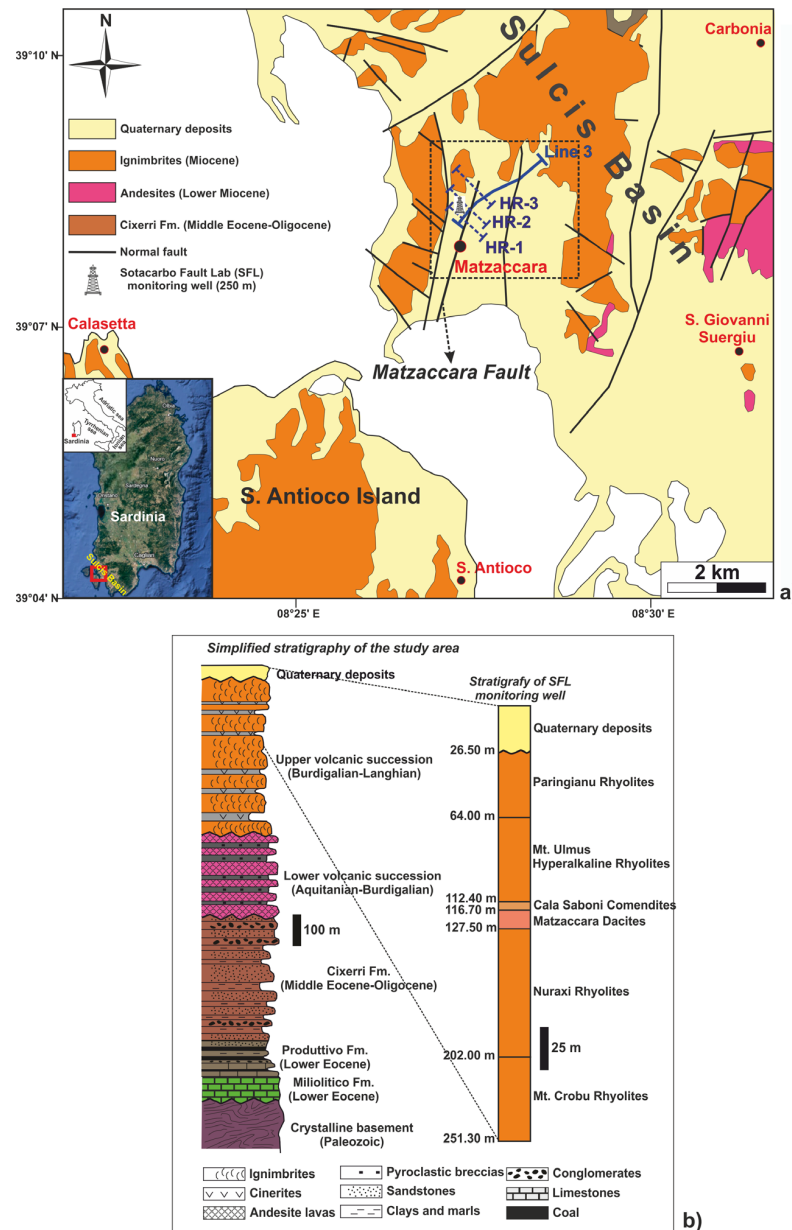
### *Matzaccara Fault*

The Matzaccara Fault was first identified through the interpretation of regional-scale seismic data acquired by OGS in the Monte Ulmus Exploration Permit in 2016 (Figure 1) [30]. Seismic data have provided an image of this tectonic structure: it exhibits normal kinematics and a listric fault plane dipping to the ESE (Figure 2). The fault affects the entire Eocene–Miocene volcano-sedimentary succession of the Sulcis coal basin and deforms the Quaternary alluvial deposits, which are characterised by a syntectonic wedge-shaped geometry, as shown by the seismic line in Figure 2.

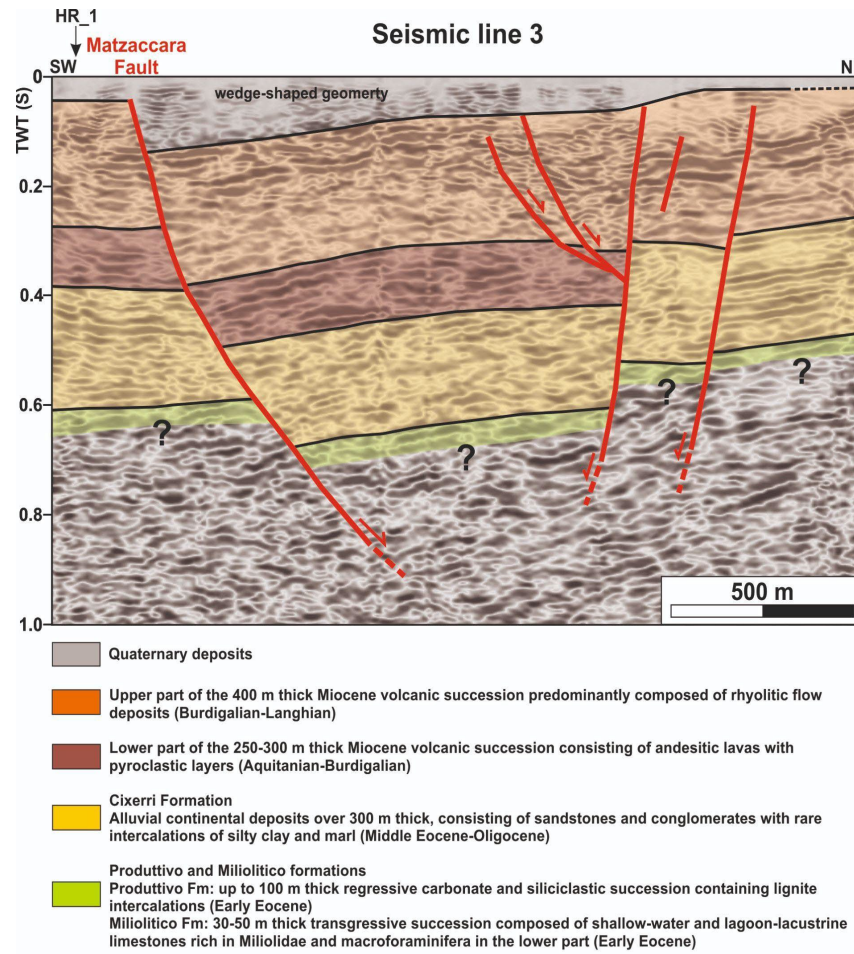
Interpretation of the HR\_1 high-resolution seismic profile (Figure 3) shows the architecture of the shallow part of the Matzaccara Fault. It consists of a fault zone with a

SE-dipping main fault plane that has a maximum vertical offset of about 60–70 m. Two synthetic subsidiary faults are recognisable in its footwall, and a sub-vertical antithetic minor structure in the hanging wall.

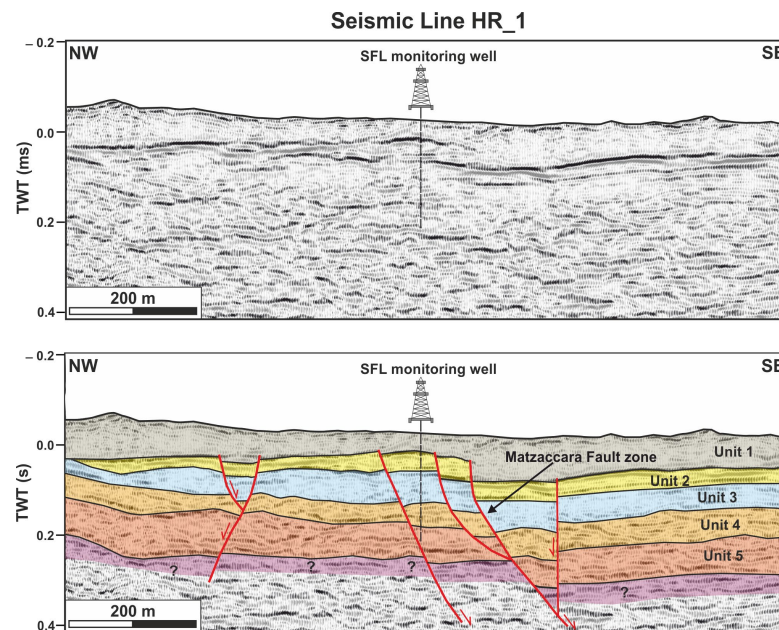
The Matzaccara Fault is an ideal candidate for studying fault behaviour as a sealing barrier or as a preferential migration pathway for CO<sub>2</sub> movement, and for testing the sensitivity of geophysical instruments for monitoring stored CO<sub>2</sub>. A specific geophysical investigation using ambient noise tomography at the SFL site revealed the presence of the fault within the first 200 m below the surface [31].



**Figure 1.** (a) Simplified geological map of the Sulcis coal basin (modified from [29]), with the location of the Matzaccara Fault. The positions of the NE–SW-oriented regional seismic profile 3 (blue solid line) and the three NW–SE-oriented high-resolution seismic lines (blue dashed lines), which were acquired in 2016 and used to characterise the Matzaccara Fault, are also reported, together with the location (black circle) of the SFL monitoring well [32]. (b) The simplified stratigraphic column of the Sulcis basin is shown, with the detailed stratigraphy of the SFL monitoring well used to interpret the seismo-stratigraphy of the high-resolution seismic profiles.



**Figure 2.** Interpretation of multichannel seismic line 3, showing the listric fault plane of the Matzaccara normal fault (location in Figure 1a). The wedge-shaped geometry of the Quaternary deposits and a graben structure are visible.



**Figure 3.** Uninterpreted and interpreted HR\_1 high resolution seismic profile crossing the Matzaccara fault zone (location in Figure 1a). Vertical scale is expressed in seconds, two-way time (TWT).

### 3. Materials and Methods

#### 3.1. High-Resolution Multichannel Seismics

In June 2016, a high-resolution seismic survey was carried out in the study area to investigate the northern part of the Matzaccara Fault, previously identified on regional seismic lines. The aim was to define the characteristics of the fault (kinematics, geometry, displacement) down to a depth of 300 m, which were initially established for the CO<sub>2</sub> injection test. The survey consisted of three NW–SE-oriented parallel seismic profiles (HR\_1, HR\_2, and HR\_3), spaced a few hundred metres apart (Figure 1a). A Vibroseis source was used for seismic acquisition. The acquisition parameters (Table 1) were calibrated to achieve optimal resolution, considering the 300 m depth target and the drilled stratigraphy composed of Miocene volcanic rocks, which, due to the presence of fractures or voids, may cause scattering and attenuation of seismic waves, and are covered by Quaternary deposits.

**Table 1.** Acquisition parameters for the seismic lines.

Source:	Minivib (upsweep 14 s, 10–240 Hz) IVI T-2500
Sensors:	geophones 10 Hz (single)
Intertraces:	4 m
Sampling:	1 ms
Time window:	16.4 s
Intershot:	8 m

The seismic data analysis revealed variability in signal-to-noise ratios across all profiles, influenced by subsoil response and noise from the nearby trunk road to Matzaccara. Processing efforts aimed to enhance signal-to-noise ratios by applying advanced techniques to attenuate both coherent and incoherent noise, and by increasing the amplitude and continuity of reflections. Tomographic inversion was performed using proprietary CAT3D software, while seismic data processing utilised ECHOS2011.3 and Seismic Unix. Two energisations per shot point were carried out and stacking of records at the same position preceded data processing. Processing steps included amplitude recovery, surface-consistent amplitude balancing, static corrections based on tomographic inversion, and various filtering techniques to improve signal quality. Dynamic corrections and migration using the Kirchhoff algorithm were applied to obtain stack and time-migrated sections (Figure 3). Seismic sections have been interpreted and visualised using IHS Kingdom<sup>®</sup> software 23.

Interpretation of the HR\_1 high-resolution seismic profile, combined with stratigraphic information from the SFL monitoring well (Figure 1b), enabled the identification of five seismic units separated by marker horizons (Figure 3). Unit 1 consists of Quaternary sedimentary deposits, while Units 2–5 form the Miocene volcanic succession. They are described as follows:

- Unit 1: The shallowest unit is bounded at the top by the ground surface and at the base by the main high-amplitude marker horizon visible in the seismic profile. This unit displays a seismic facies characterised by sub-parallel, inclined, and undulating high-frequency reflectors with poor lateral continuity and low amplitude. Local downlap terminations against the marker reflector are evident. The thickness ranges from about 50 to 100 ms, corresponding to 30 to 60 m, assuming an interval velocity of 1200 m/s. The maximum thickness occurs in the hanging wall of the main fault plane of the Matzaccara fault zone;
- Unit 2: This unit comprises continuous high-amplitude reflectors deformed by the Matzaccara fault zone and secondary normal faults (Figure 3). The thickness is roughly

constant, ranging between 30 and 50 ms, which corresponds to approximately 30 to 50 m, assuming an interval velocity of 2000 m/s for the entire volcanic succession crossed by the seismic profile;

- Unit 3: This unit consists of low-frequency, generally low-amplitude, sub-horizontal to inclined discontinuous reflectors (Figure 3). The minimum thickness, about 60 ms (60 m), is observed in the north-westernmost part of the line, where the inclined reflectors are truncated by the base of Unit 2. Elsewhere along the line, the thickness is roughly constant at about 80–110 ms (80–110 m);
- Unit 4: This unit consists of low-frequency, low- to high-amplitude, sub-horizontal discontinuous reflectors and has an approximately constant thickness of 100–110 ms (100–110 m) (Figure 3);
- Unit 5: The deepest unit consists of low-frequency, medium- to high-amplitude, sub-horizontal to undulating discontinuous reflectors. The maximum thickness, about 200 ms (200 m), is observed in the north-westernmost sector of the line.

### 3.2. Feasibility Study

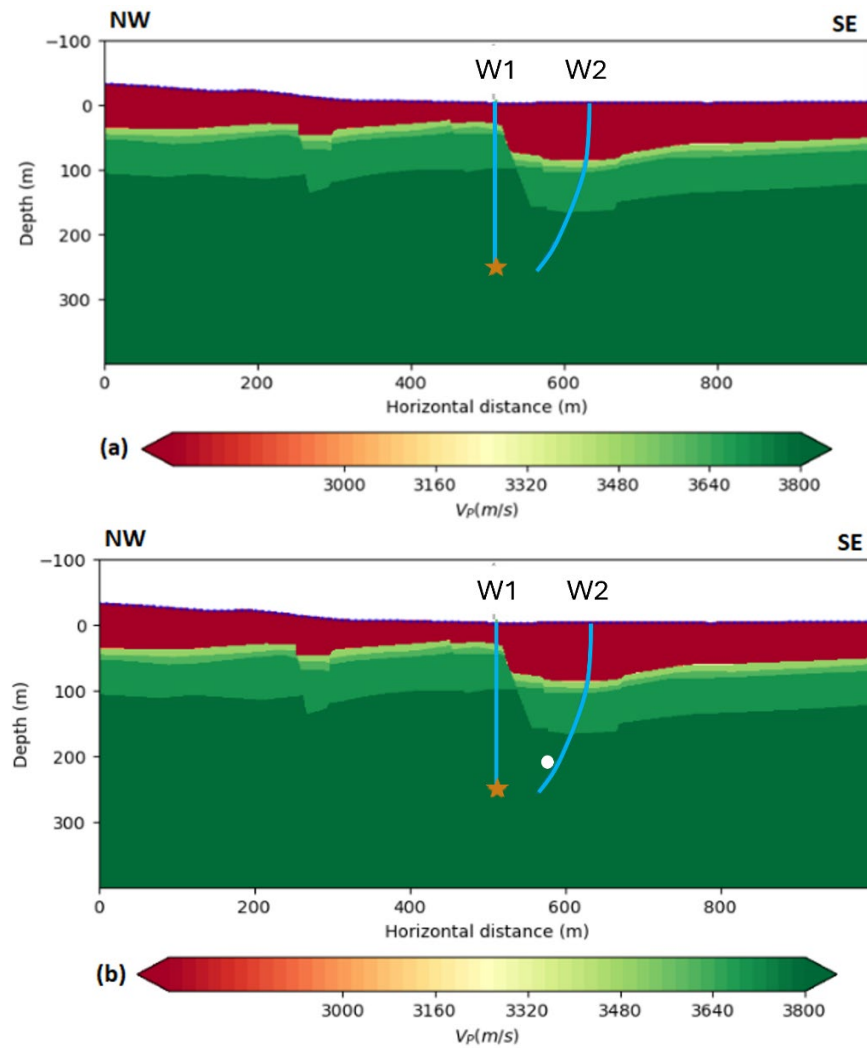
The feasibility study aimed to assess the potential of geophysical methods for detecting injected CO<sub>2</sub> along the target fault and to determine the optimal parameters for planning the geophysical survey, thereby improving the site's overall characterisation. This characterisation was essential in order to identify a suitable location for the planned injection well, complementing the monitoring well, to ensure proper CO<sub>2</sub> injection within the fault and to investigate its migration behaviour along the fault zone.

Elastic seismic full-waveform simulation was used to assess the effect of CO<sub>2</sub> injection on the propagation of seismic waves, particularly focusing on potential observations in a time-lapse acquisition before and after CO<sub>2</sub> injection. A 2D geological model was built based on the available data, and a preliminary geological interpretation was formulated and then revised. The simulation was run with the vertical monitoring well (W1) and assumed a deviated injection well (W2) to intercept the fault within the planned 250 m drilling length. The wells are located on opposite sides of the interpreted fault (see Figure 4). The model had dimensions of 1000 × 500 m and was discretised using square pixels with a side length of 0.5 m. Both crosswell (CW) and surface acquisitions were simulated using seismic sources positioned in the vertical well and receivers for the CW acquisition were placed every 1 m in the injection well and at the surface. A Ricker wavelet with a 400 Hz cut-off frequency was used as the vertical synthetic source to remain within the Gassmann approximation. Several sources and CO<sub>2</sub> injection positions were tested; the best results were obtained from the source located at 250 m and are presented here.

#### 3.2.1. Theory

From a seismic perspective, the injected CO<sub>2</sub>, which replaces water as the interstitial fluid, alters the bulk modulus of the saturated rock, thereby modifying the velocity at which compressional (P) waves propagate through the medium. In the model, the pore fluid in the pre-injection phase is water, which is subsequently replaced by CO<sub>2</sub> upon injection.

To compute the bulk and shear moduli ( $K_{sat}$ ,  $\mu_{sat}$ ) of the porous fluid-saturated medium, Gassmann's relations were applied. The Gassmann relations are derived under the assumption of low-frequency or quasi-static conditions, where fluid pressure within the pores has sufficient time to equilibrate across the pore space [33]. The validity of the Gassmann relation is typically controlled by Biot's characteristic frequency ( $f_c$ ), which separates low-frequency (quasi-static) from high-frequency (dynamic) behaviour and depends on the porosity and permeability of the rock and the dynamic viscosity of the fluid. For low- to medium-permeability rocks, ( $f_c$ ) can range from 10 Hz to more than 1 kHz.



**Figure 4.** Models used to simulate waveform propagation (a) before and (b) after injection. The colour bar shows the variation in  $V_P$  velocity in the modelled  $\text{CO}_2$  sphere in (b) (depth 190 m, 6 m radius circle close to the deviated well and the interpreted fault). The source position is represented by the star. Receivers are placed at the surface and in the planned deviated well (blue line) in the CW acquisition layout, respectively.

The fluid-saturated bulk and shear moduli are given by [34], as follows:

$$K_{sat} = K_{dry} + \alpha^2 \left[ \frac{K_{solid}}{\alpha - \phi + \phi \cdot \frac{K_{solid}}{K_{fluid}}} \right]$$

$$\mu_{sat} = \mu_{dry},$$

where  $\phi$  is the porosity of the host rock,  $K_{dry}, \mu_{dry}$  are the drained bulk and shear modulus, respectively,  $K_{solid} = V_{P_{solid}}^2 \cdot \rho$  is the bulk modulus of the solid phase of the rock,  $\alpha = 1 - \frac{K_{dry}}{K_{solid}}$  is the Biot's coefficient, and  $K_{fluid}$  is the bulk modulus of the pore fluid, which depends on the reservoir pressure and temperature conditions.

The complex compressional and shear saturated rock wave velocities are stated as follows:

$$c_P = \sqrt{\frac{K_{sat} + \frac{4\mu_{sat}}{3}}{\rho_m}} \text{ and } c_S = \sqrt{\frac{\mu_{sat}}{\rho_m}}$$

from which, for homogeneous waves in isotropic media, we obtain the phase velocities as follows:

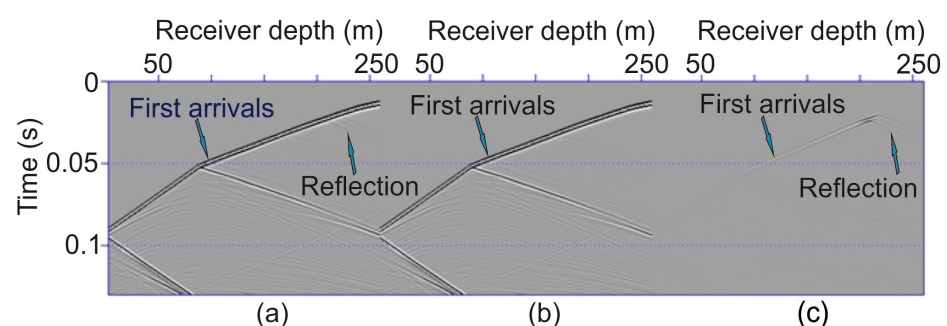
$$V_P = \left[ \operatorname{Re} \left\{ \frac{1}{c_P} \right\} \right]^{-1} \quad \text{and} \quad V_S = \left[ \operatorname{Re} \left\{ \frac{1}{c_S} \right\} \right]^{-1}$$

The density of the porous medium is  $\rho_m = \phi \rho_f + (1 - \phi) \rho_s$ , where  $\rho_f$  is the pore fluid density. At frequencies where the Gassmann relation is valid, we can expect a change in the P-wave velocity of the saturated rock in the area affected by the injection, which can result in changes in the seismic signal acquired before and post CO<sub>2</sub> injection.

### 3.2.2. Crosswell and Surface Numerical Simulations

According to the information available at the time, the velocity model of the NW–SE line shown in Figure 4a was derived. In the crosswell simulation, the source was placed in the monitoring well at a depth of 250 m, and receivers were positioned every 1 m in the injection well. The injected CO<sub>2</sub> plume was considered at a depth of about 190 m in the injection well (W2). The radius of the simulated sphere was calculated as if 5.5 tonnes of CO<sub>2</sub> were injected (radius = 6 m, Figure 4b). The geophysical properties of the host layer were set as follows: P-wave velocity of the host rock solid phase  $V_{P_s} = 3800$  m/s, density computed with Gardner's relation  $\rho_s = 2300 \text{ kg m}^{-3}$ , compressional to shear wave velocity ratio of 2, Biot's coefficient  $\alpha = 0.36$ , and porosity  $\phi = 0.09$ . The density, acoustic velocity, and bulk modulus of the fluids (water and CO<sub>2</sub>) were computed at the corresponding reservoir pressure and temperature conditions ( $P = 30$  atm,  $T = 18$  °C), using CoolProp codes [35] based on the thermophysical database provided by the National Institute of Standards and Technology (NIST).

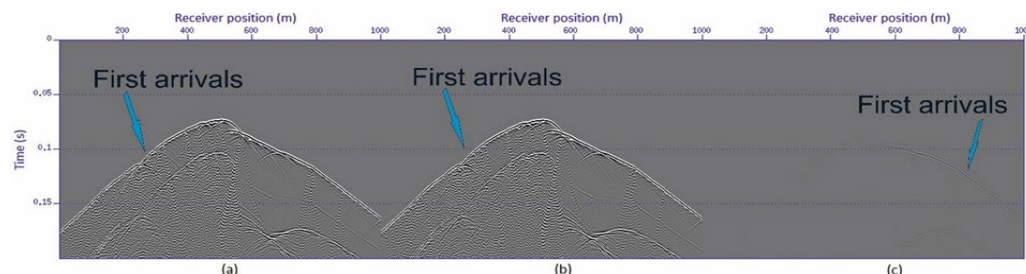
Elastic full-waveform propagation in the crosswell configuration was simulated, and the resulting synthetic pressure components are shown in Figure 5, with consistent amplitude normalisation across the three panels. The seismograms show the signals after CO<sub>2</sub> injection (Figure 5a) and before injection (Figure 5b), and the difference between the two is shown in Figure 5c. Although the amplitude of the difference signal is relatively low compared to the full synthetics, clear reflections from the boundaries of the CO<sub>2</sub> plume are visible in the receivers below 200 m depth in Figure 5a and become particularly evident in the difference panel (Figure 5c).



**Figure 5.** Pressure components acquired in crosswell configuration after CO<sub>2</sub> injection (a), before injection (b), and as the difference between the two (c).

The synthetic signals recorded at the surface (Figure 6) were also acquired from the source located at a depth of 250 m in the monitoring well. As expected, the configuration with surface receivers, while keeping all other modelling parameters unchanged, proved less effective than the crosswell configuration in detecting changes associated with the CO<sub>2</sub> plume. The seismograms after injection (Figure 6a) and before injection (Figure 6b), and the difference (Figure 6c), are displayed using the same amplitude normalisation, but with a higher global gain compared to the crosswell configuration (Figure 5). The

difference signal is barely visible, particularly for receivers located to the right of the plume. In Figure 6c, the presence of CO<sub>2</sub> affects the first arrivals, but the effect on the reflection is not visually detectable in this type of acquisition geometry. These results suggest that seismic monitoring in a crosswell configuration is preferable, especially if the injection well is equipped with permanent instrumentation such as distributed acoustic sensing (DAS), which provides highly dense spatial resolution [36,37].



**Figure 6.** Vertical particle velocity components acquired in crosswell configuration after CO<sub>2</sub> injection (a), before injection (b), and as difference between the two (c).

### 3.3. Borehole Geophysical Study

Following the modelling of the initial feasibility study and the high-resolution seismic investigations, borehole seismic surveys were conducted for SFL to characterise the Matzaccara Fault and its surrounding area, as a baseline for CO<sub>2</sub> injection testing.

The opportunity to perform borehole geophysical surveys arose from the presence of the monitoring well W1 (SFL monitoring well) close to the main fault (Figure 7). To avoid electrical interference, the vertical well W1 was cased to a depth of 250 m with a fiberglass casing suitable for geoelectrical surveys, with electric resistivity tomography (ERT) cables installed on the exterior of the casing [38]. Vertical seismic profiles (VSPs) are geophysical measurements made in a wellbore, using geophones positioned at depth inside the wellbore and a seismic source at the surface, typically near the well. The seismic source generates acoustic waves that are recorded by the geophones in the well. VSPs offer significant advantages over surface seismic surveys; VSP data have higher resolution, as the wave path is shorter (receivers are in the well), and they provide a direct correspondence between time and depth, which is used to calibrate the surface seismic data. Furthermore, VSPs provide interval velocities in depth along the well, giving indications about the type of formations encountered from a seismic perspective. The data collected in 2019–2020 by VSP, jointly analysed with resistivity data from the geoelectric survey, provided useful indications of the possible location of the injection well, which was planned to be drilled in 2023.

The geophysical surveys consisted of the following:

1. Two near-offset vertical seismic profiles (VSPs);
2. Multi-offset VSPs (several VSP surveys with the source moving along offset) in well W1 and in a shallower piezometric well 65 m from W1;
3. A geoelectrical survey with electrodes located both in the well and at the surface.

The results of the two near-offset VSPs from the vertical component data, the resistivity model from ERT, and the joint data integration of these two complementary methodologies are described below.

In this study, well logs were not available, apart from laboratory measurements carried out on selected cores taken during the drilling of the monitoring well W1. Well logs provide punctual information on physical parameters along the well, providing a constraint for other seismic/geophysical methods. In this work, integrated use of surface seismic data, VSPs, and ERT provides a multi-scale and multi-physics approach to fault characterisation

that overcomes the limitations of any single method. Surface seismic data define the regional fault architecture, including fault location, geometry, and continuity, forming the structural framework of the site of interest. VSPs refine this framework near wells by improving depth accuracy and imaging faults below the resolution of surface seismic data. If well logs are available, they provide direct measurements of lithology, elastic properties, porosity, permeability, and fault-zone characteristics. Together, seismic data and well logs constrain fault geometry, sealing potential, and mechanical behavior with higher confidence. With regard to CO<sub>2</sub> injection, this integrated dataset is critical for evaluating containment and operational risk. Well logs and seismic data inform assessments of caprock integrity and fault sealing capacity, VSPs ensure accurate positioning of faults relative to injection intervals, and ERT adds sensitivity to fluid distribution by detecting resistivity changes associated with CO<sub>2</sub> replacing brine. Time-lapse seismic/VSP and ERT monitoring can track CO<sub>2</sub> migration and identify movement toward faults, enabling early detection of leakage pathways and supporting safe injection pressure, rate design, and long-term storage security.

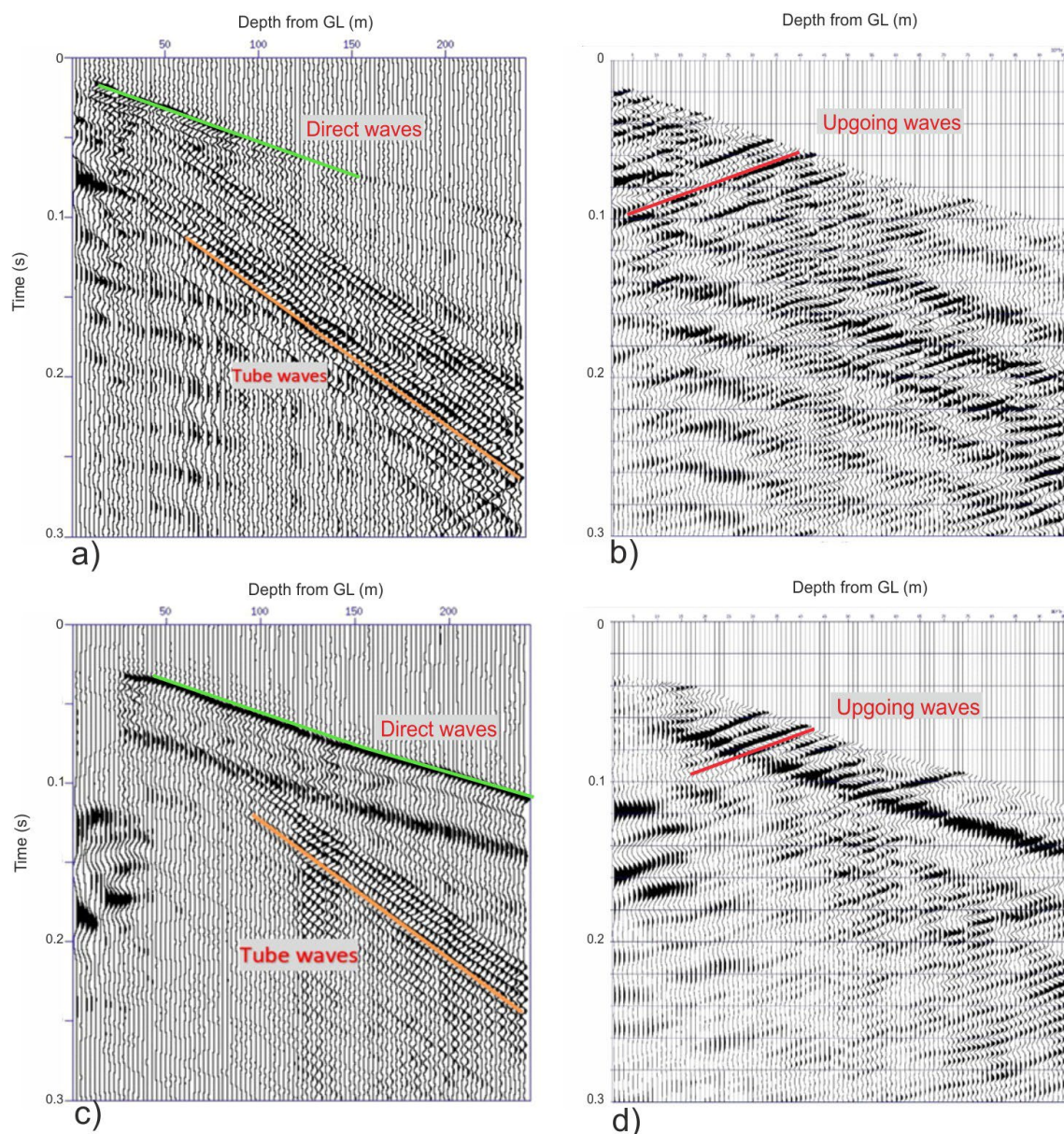


**Figure 7.** Map showing the position of the well W1 and the positions of the seismic source for the first near-offset VSP (Shot Point 510) and the second near-offset VSP (Shot Point 530).

### 3.3.1. Near-Offset VSPs

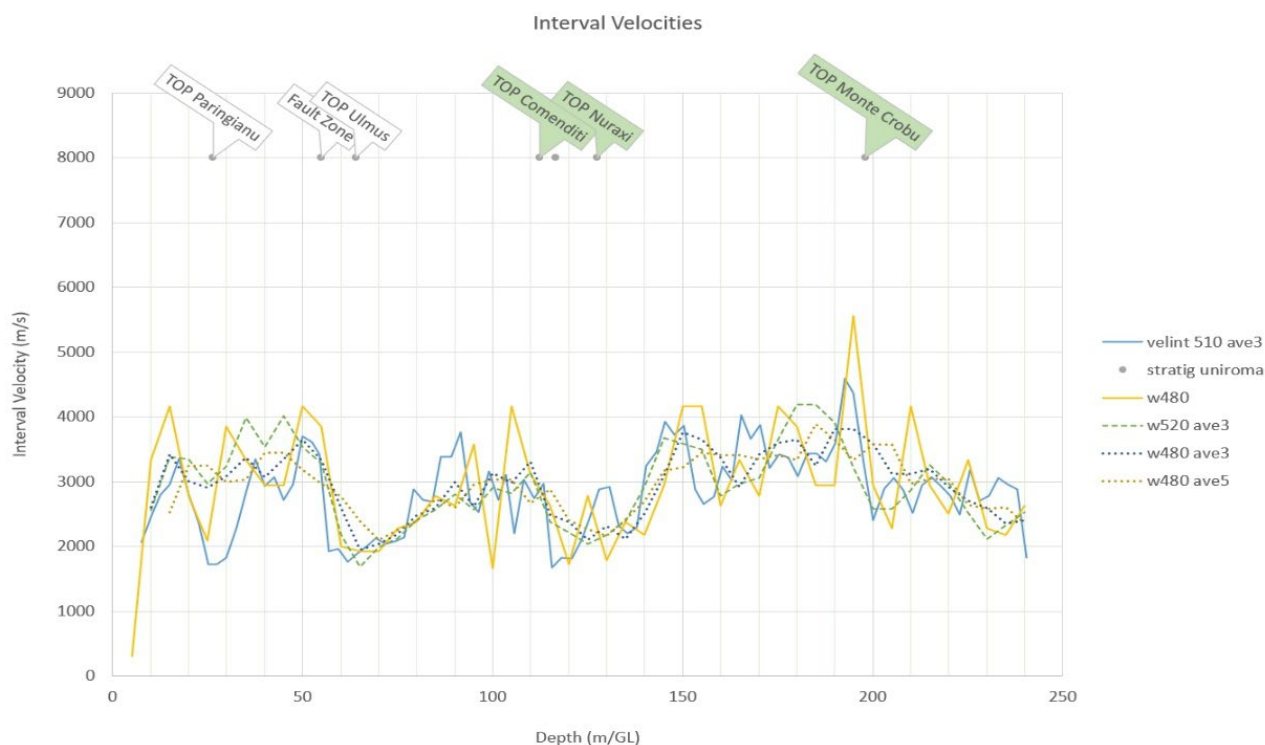
The two near-offset VSPs were conducted in February 2020 at 10 m (SP 510) and 30 m (SP 530) offset south-east from well W1, respectively (Figure 7). The surveys were performed using an Avalon 3C geophone, capable of recording the vertical and horizontal components of the different wavefields, from 5 m to 240 m depth along the well. The source was an IVI Minivib Vibroseis, driven by a Seismic Source Force III control system, which included encoder and decoder units installed on the Vibroseis and in the control cabin, respectively, where the time break signal for the sweep start was delivered and the reference signals (the pilots) were fed into the acquisition system. The Minivib operated in P mode, using a sweep from 10 Hz to 320 Hz. The spatial sampling of the receivers in the well was 2.5 m.

The VSP 510 was strongly dominated by tube waves (Figure 8a), generated by the source very close to the well, and interface waves traveling along the steel-cased borehole, along the interface between the fluid in the wellbore and the wall of the wellbore. Starting from the picking of the first arrivals of the total wavefield, the one-way traveltime (OWT) upgoing wavefield, representing the reflections from the subsurface, was recovered by wavefield separation (Figure 8b). The wavefield separation enhanced the upgoing events and partially attenuated the tube waves. In addition, we applied an F-K filter to further attenuate the tube waves and better highlight the reflections. The total wavefield of VSP 530 was less dominated by tube waves, as the source was located farther from well W1 (Figure 8c). Figure 8d shows the corresponding OWT upgoing wavefield.



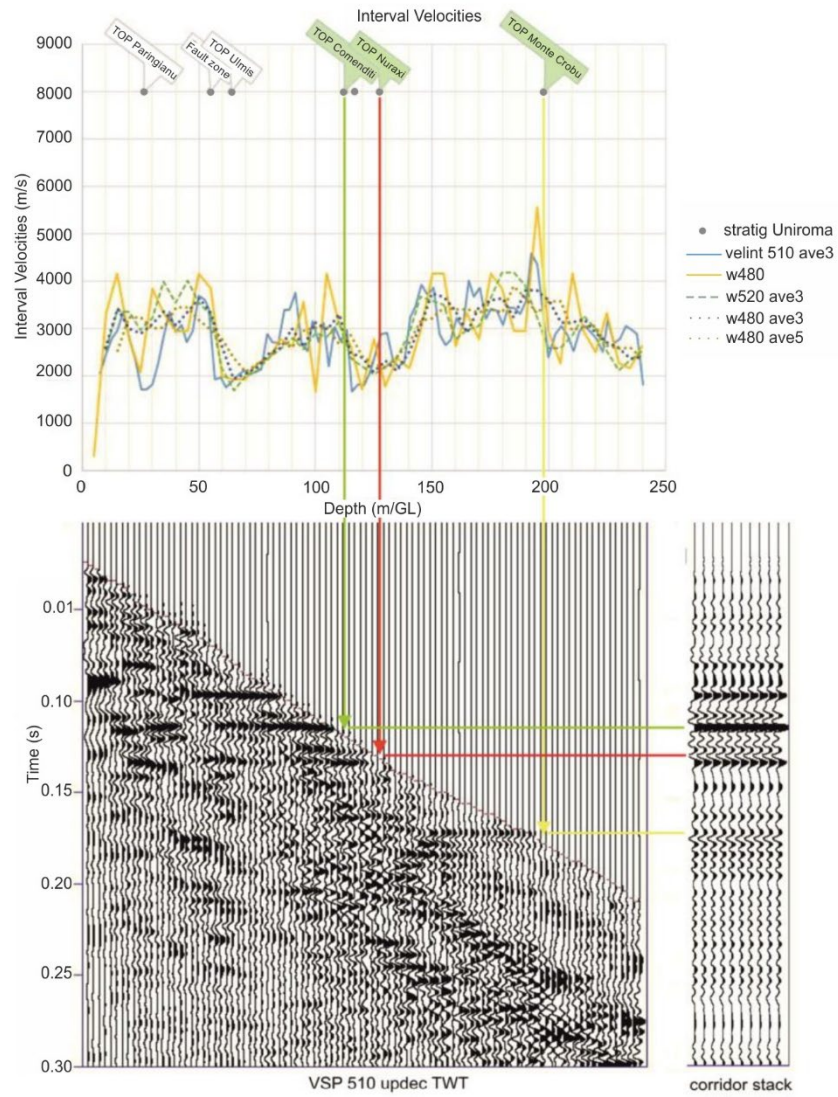
**Figure 8.** Comparison between VSP 510 (above) and VSP 530 (below). (a) Total wavefield of VSP 510 strongly dominated by tube waves and (b) corresponding OWT upgoing wavefield after wavefield separation. The tube waves are attenuated by a F-K filter and the reflections from the subsurface are visible. Data are not bandpass filtered. (c) Total wavefield of VSP 530. The data are less dominated by tube waves, because the source was located farther from the well. (d) Corresponding OWT upgoing wavefield after wavefield separation. The tube waves are attenuated and the reflections from the subsurface are visible. Data have not been bandpass filtered.

Using the first arrivals from the VSP data, the interval velocities of the geological formations across the well were calculated. Figure 9 illustrates the interpretation of formation tops in relation to changes in the velocity function with depth.

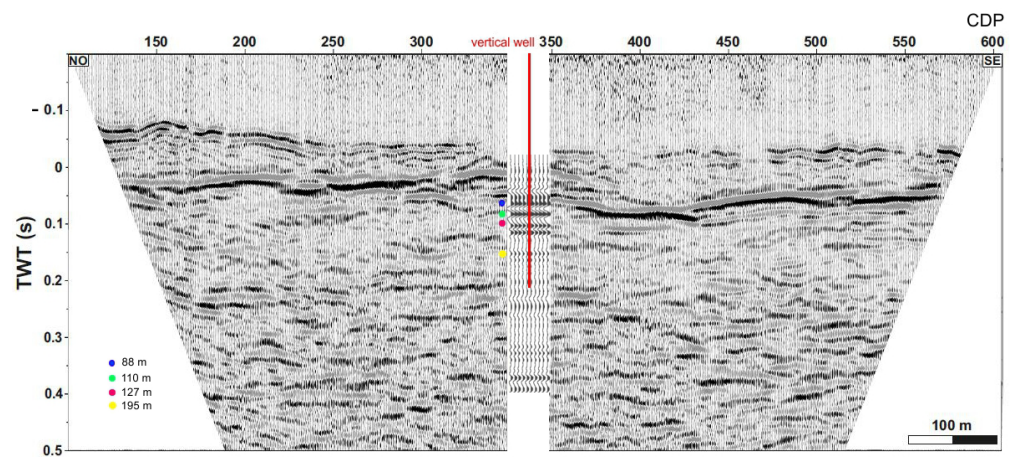


**Figure 9.** Interval averaged velocities from VSP 510 (blue solid line). The velocity trends are confirmed by other two VSPs (VSP 480 and VSP 520) from the multioffset survey with hydrophones in W1.

Figures 9 and 10 show that three of the interpreted formation tops from the calculated interval velocities align with the reflections observed in the two-way traveltime (TWT) VSP 510 upgoing wavefield. However, the quality of data for shallower reflections is compromised by the presence of unconsolidated sediments or weathering, making reliable interpretation difficult. Figure 10 also presents the TWT corridor stack derived from the data, which visually enhances the reflections. The VSP data facilitate the calibration of seismic reflection, linking the TWT reflectors of the stack section to the corresponding depths. This enables comparison of the VSP results with the HR1 reflection seismic stack time section (Figure 10), which is closest to well W1 (see map in Figure 1). The stack section was divided, and the corridor stack was positioned at the corresponding projected well location on the line (Figure 11). Using the time-depth correspondence in the VSP from Figure 10, the depth of the signal in time was directly determined. This information is shown in Figure 11, where the coloured circles along the corridor stack indicate the depth of the selected reflectors in the stack section. The formation at the depth of the green circle is interpreted as the top of Comenditi, the one at the depth of the red circle as the top of Nuraxi, and the one at the depth of the yellow circle as the top of Monte Crobu. The blue signal has not been assigned to a specific top formation, as it appears clearly in the corridor stack from the VSP but cannot be resolved by the seismic data due to its very thin thickness.



**Figure 10.** Composite figure showing how the variations in the interval velocities (**up**) fit with the reflections in the TWT VSP data (**below**, on the left). The corridor stack on the right is used for comparison with the seismic reflection (Figure 11).



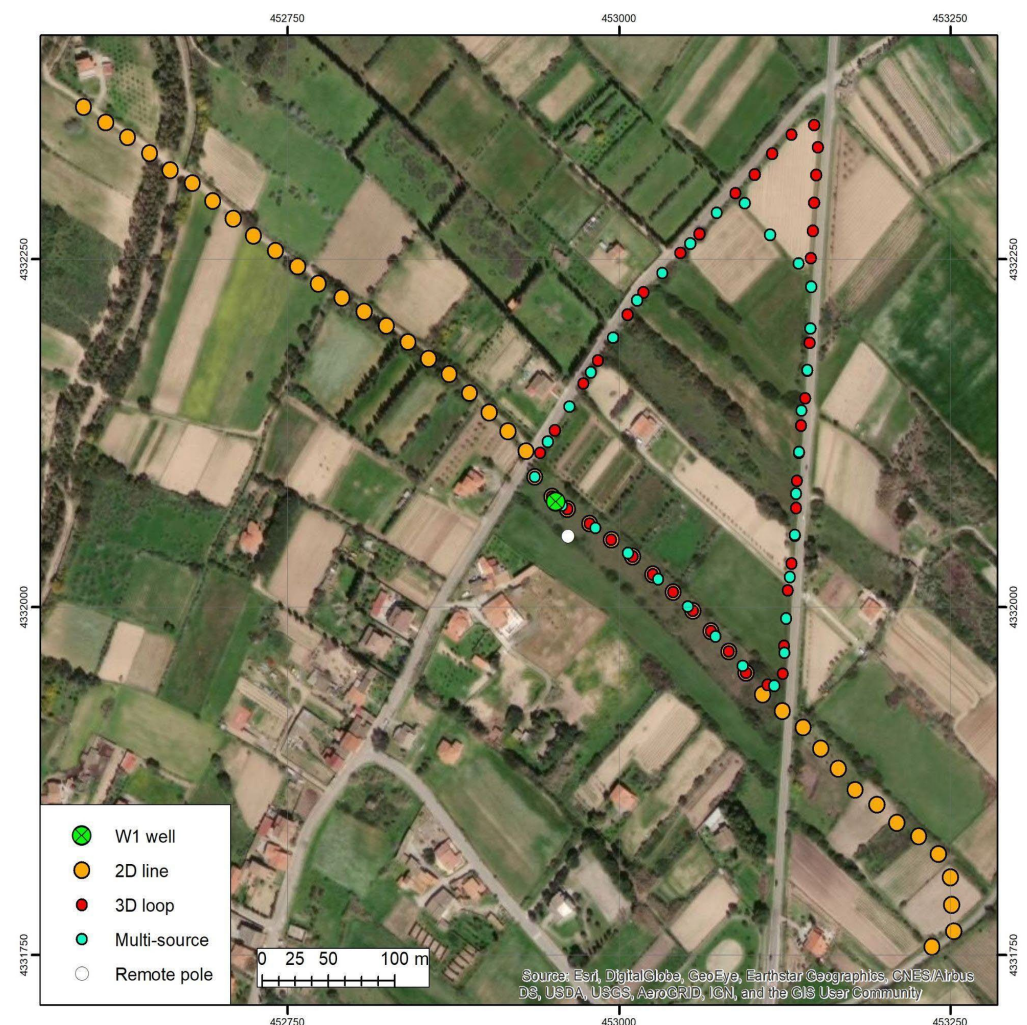
**Figure 11.** Stack section of line HR1. The corridor stack from near offset data (VSP 510) has been inserted at the position of W1 well on the line after the section was split.

### 3.3.2. Electric Resistivity Tomography (Ert)

Integration of different methodologies increases the reliability of the results. For this purpose, in addition to the two seismic methods (surface seismic surveys and VSPs), an electrical survey was conducted. Electrical resistivity tomography (ERT) is a non-invasive geophysical method for investigating the subsurface by examining the electrical properties of geological formations. It assumes that different entities, such as minerals, solid bedrock, sediments, air-filled, and water-filled structures, exhibit detectable contrasts in electrical resistivity compared to the host medium [39].

In December 2019, 2D and 3D ERT surveys were carried out at SFL, both surface and surface–borehole, where observation well W1 was already equipped with 48 electrodes spaced at approximately 5 m intervals [38]. The first four electrodes were not used in the acquisition due to the presence of steel casing in the upper part, while the remainder of the well had a fibreglass casing, as previously described.

The 2D surface profile, oriented NW–SE and 920 m in length, consists of 48 electrodes spaced 20 m apart and follows the seismic line HR\_1 (Figure 12).



**Figure 12.** Field survey position map with electrode distribution and position of well W1. All the data described were acquired in collaboration with Geostudi Astier by using their multi-electrode system SYSCAL Pro 96 resistivitymeter.

Three different geometries were used for the 2D acquisition, as follows:

- (1) Wenner–Schlumberger 2D surface profile;
- (2) Wenner–Schlumberger along the borehole;

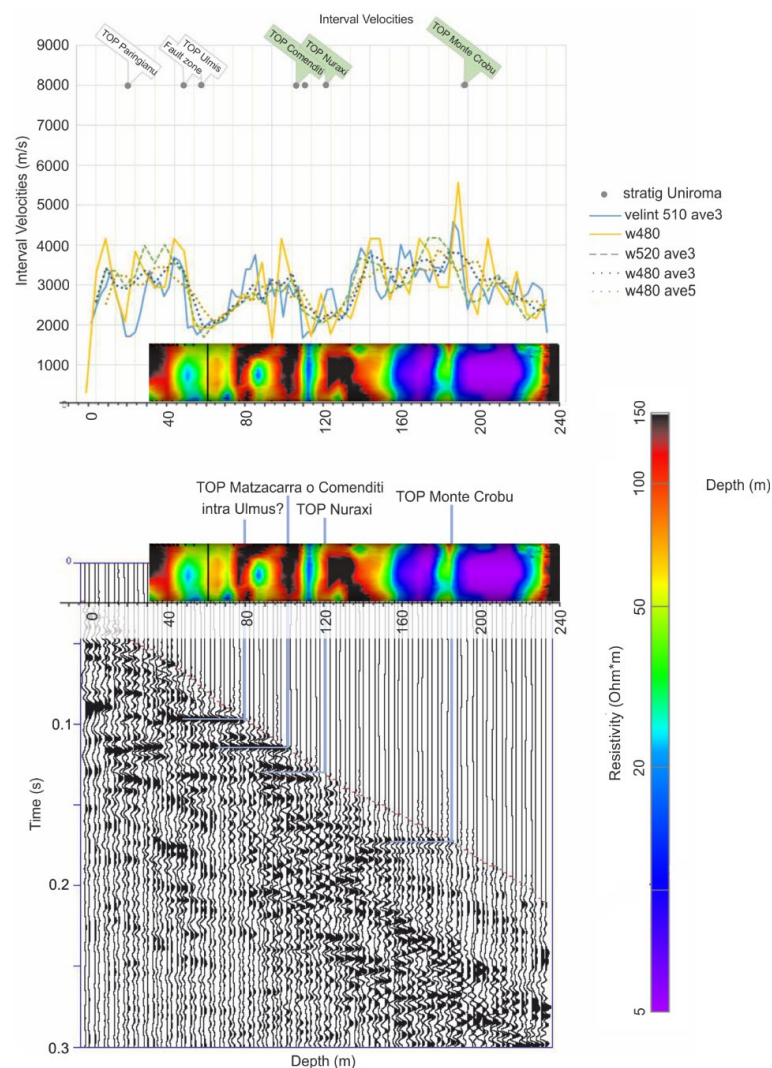
(3) Surface-to-borehole dipole–dipole between the 2D surface profile and the borehole.

The 3D acquisition forms a triangle designed along the roads to achieve the best response for the survey with minimal impact on the population. One side of the triangle corresponds to part of the 2D profile. All survey acquisition geometries are shown in Figure 12.

### Data Inversion

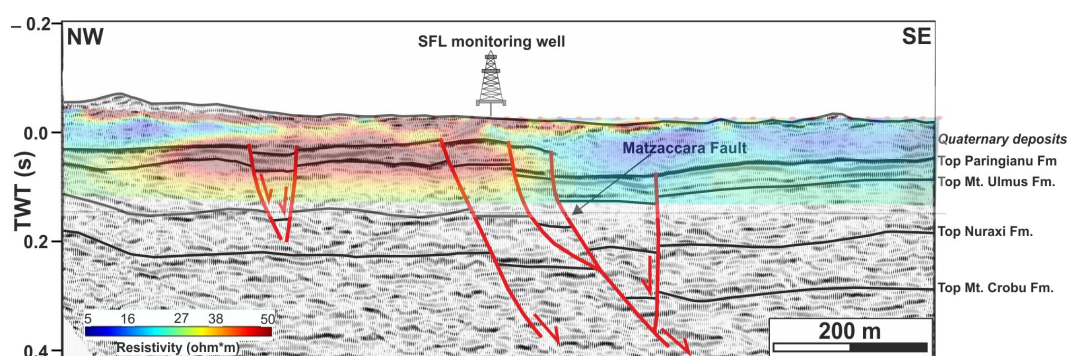
The collected data were inverted by OGS using ERTLab64 1.2 software by Geostudi Astier, for both single acquisitions and combined datasets. The primary objective at this stage of the project was to enhance the available information in the area between the observation well and the planned injection well. Useful information was obtained exclusively from the 2D and 3D surface surveys, as the data inversions from borehole electrodes produced unreliable higher-resistivity values compared to the surface data, obscuring the resistivity values of deeper formations.

A preliminary 1D profile was constructed from resistivity data collected across the well. To validate this profile, it was compared with both the VSP TWT upgoing wavefield and the velocity profile (Figure 13). The joint interpretation shows good correspondence between changes in resistivity and the velocity function (on the right), confirmed by changes in the lithostratigraphy identified by the VSP interpretation (on the left).



**Figure 13.** Joint interpretation of the VSP profile and the 1D resistivity borehole profile.

The comparison between the 2D resistivity profile and the HR\_1 seismic section (Figure 14) shows a strong correlation between the resistivity variations and the geological interpretation. Notably, in the Matzaccara fault zone, a distinct shift in the resistivity pattern can be observed. Higher resistivity values are present to the left of the monitoring well, while these values decrease towards the right, or southeast. The topmost layer corresponds to Quaternary alluvial deposits (Figure 1), and the variation in resistivity is probably not due to changes in lithology but rather to the presence of the fault. In fault zones, particularly on the hanging wall, increased fracturing is common, leading to higher porosity compared to the surrounding rock. This enhanced porosity facilitates fluid accumulation, which may result in the formation of a “fault gouge”—a zone of finely crushed rock material within the fault. Fault gouge typically exhibits lower resistivity than the surrounding rock due to its finer grain size, higher porosity, and greater likelihood of being saturated with conductive fluids. This observation supports the conclusion that the Matzaccara Fault has been recently active, influencing the characteristics of the Quaternary deposits.



**Figure 14.** Wenner–Schlumberger 2D surface resistivity profile superimposed on the HR1 interpreted seismic section.

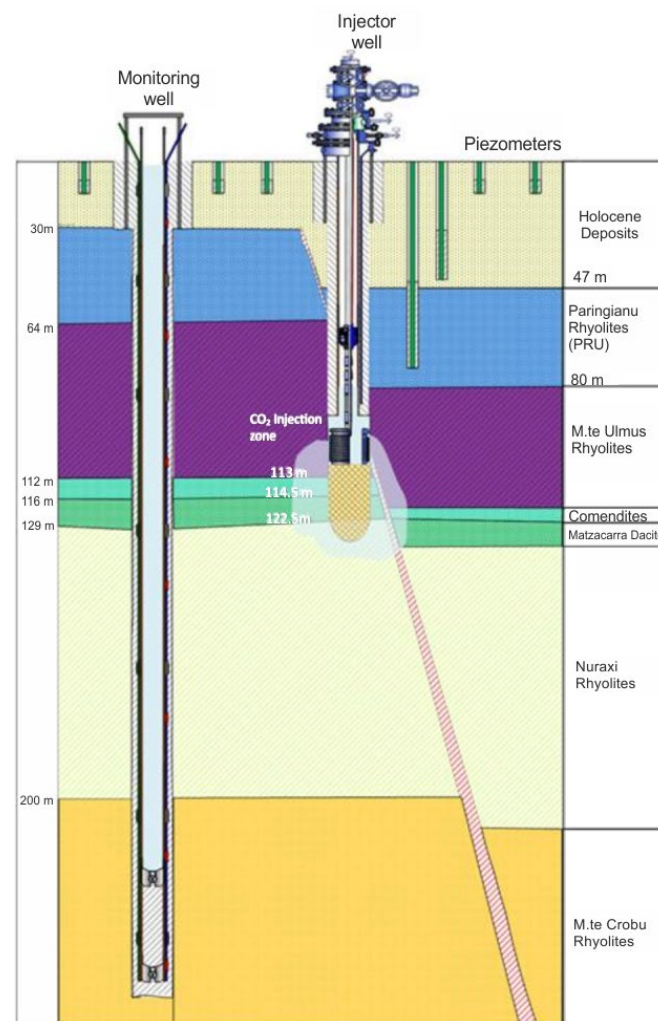
#### 4. Results

By integrating geophysical and well log data with geological information from the geological map sheet no. 564 “Carbonia” [20,29] and the SFL monitoring well, the seismic section was interpreted as follows:

- Unit 1 represents the Quaternary alluvial deposits;
- Unit 2 represents the uppermost part of the volcanic sequence, deformed by the Matzaccara fault zone and secondary normal faults. This unit correlates with the Langhian Paringianu Rhyolites Formation, which consists of pyroclastic fall and flow deposits (tuffs and lapilli);
- Unit 3 is associated with several Langhian pyroclastic volcanic formations, such as the Hyperalkaline Rhyolites of Mt. Ulmus, Cala Saboni Comendites, and Matzaccara Dacites;
- Unit 4 is associated with the Langhian Nuraxi Rhyolites Formation, consisting of densely welded pyroclastic flow deposits;
- Unit 5 is the deepest unit and is associated with the Burdigalian–Langhian Mt. Crobu Rhyolites Formation, composed of densely welded pyroclastic deposits.

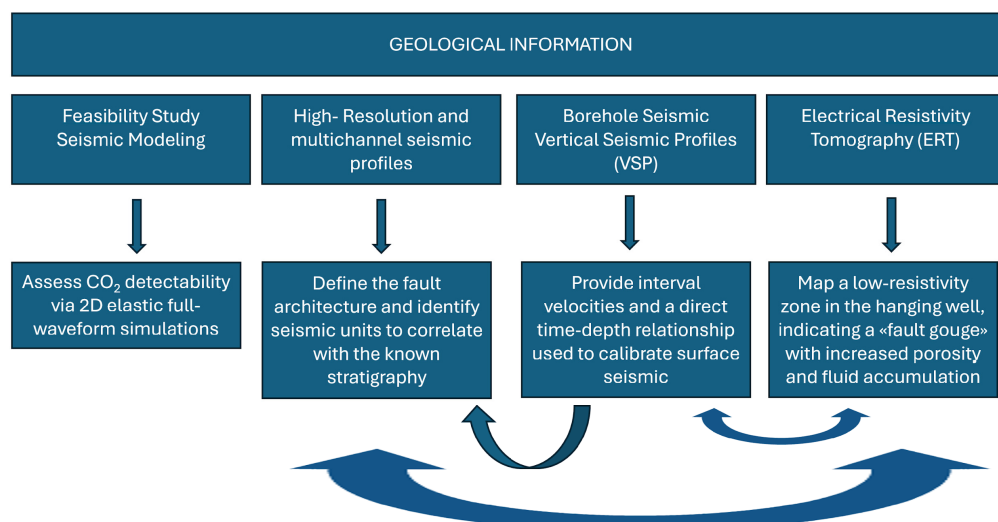
The previously described site characterisation provided detailed information for the design of the injection well (Figure 15). Unlike the plan in the feasibility study simulation, the injection well was drilled vertically; however, this did not affect the validity of the modelling results for the geophysical studies conducted. The well was drilled in the hanging wall of the fault, passing through the Holocene sandy deposit to a depth of 47 m and reaching the top of the upper rhyolitic rock (Paringianu Fm.). The fault was intercepted

at a depth of about 100 m. The injection well is equipped with a 5½" (140 mm) fibreglass casing (selected to prevent electrical interference with the ERT cables installed outside the casing), which houses the injection pipes and allows monitoring probes to be introduced into the well. In parallel, a fibre optic cable was run from the casing shoe to the surface to enable monitoring of gas migration in the rock above the injection point. Standard class G cement was used to cement the casing and the cable in place, isolating groundwater and minimising potential leakage pathways along interfaces between well casings and geological formations and along cables, thus ensuring that CO<sub>2</sub> only leaks through the soil and the fault. Pressure, temperature, geoelectrical, geochemical and seismic data can be collected, processed, and analysed during the injection tests. In addition, two downhole pressure and temperature transmitters (DPTT) have been installed to provide accurate measurements at the bottom of the well in the injection zone (Figure 15).



**Figure 15.** Scheme of the actual well configuration of the SFL test bed.

To summarise the work carried out and to clarify the study methodologies and the chronological sequence that led to the results presented, we present the workflow shown in Figure 16. The diagram shows how the available well data (from the monitoring well) and the geological model derived from geological data were used to identify the Matzacarra Fault, which was subsequently characterised and represents the structure underlying the creation of the SFL test site.



**Figure 16.** Flowchart of the SLF test site characterisation.

A feasibility study based on modeling CO<sub>2</sub> injection near the fault made it possible to assess the seismic response and to accordingly calibrate the acquisition parameters of the seismic methods applied later. High-resolution seismic reflection surveys allowed the definition of fault geometry the detection of the seismic units. Thanks to the velocity functions obtained from the VSP, these units were correlated with specific known formations, and their depths and thicknesses were determined (and also validated by electrical tomography). These results were then used for the siting and design of the injection well.

## 5. Discussion

This study demonstrates the use of integrated geophysical techniques to characterise the CO<sub>2</sub> Sulcis Fault Lab (SFL) test site, located in the southern part of the Sulcis coal basin in Sardinia. The site was selected to investigate the behaviour of CO<sub>2</sub> in the presence of faults. It is characterised by a several hundred metres thick Miocene volcanic sequence, a type of rock that generally produces a weak seismic response. Therefore, a feasibility study was conducted to assess the potential of geophysical methods to detect injected CO<sub>2</sub> along the target fault, the Matzaccara Fault, identified by regional-scale seismic reflection profiles, and to determine the optimal acquisition parameters for survey planning, thereby improving the overall site characterisation. The regional-scale seismic profiles show that the fault also affects the Quaternary deposits. High-resolution seismic profiles acquired along the fault trace were essential for defining the kinematics, geometry, and displacement associated with the Matzaccara Fault. The seismic investigation reached depths of approximately 300 m, slightly beyond the planned CO<sub>2</sub> injection depth. Five seismic units have been identified. The shallowest consists of Quaternary deposits overlying the Miocene volcanic sequence, which is mainly composed of rhyolites, as well as comendites and dacites. The data provide a detailed image of the architecture of the Matzaccara fault zone, which consists of a SE-dipping main fault plane with a normal offset of approximately 50–60 m, two synthetic minor faults in the footwall, where the SFL monitoring well is located, and a sub-vertical antithetic structure in the hanging wall. The deformation of Quaternary alluvial deposits with a syntectonic wedge-shaped geometry indicates that the Matzaccara Fault can be considered as a recent fault in the southern Sulcis basin. Therefore, by studying its behaviour in relation to CO<sub>2</sub> injection, it will be possible to hypothesise the behaviour of older tectonic structures in the area. Moreover, the seismic data provided crucial information for subsequent investigations, including the definition of acquisition parameters for borehole geophysics and planning the injection well. VSP data provided

interval velocities for the geological formations intersected by the well. These velocities enabled the construction of a time–depth relationship used to align seismic reflections (in two-way travel time) with the lithological tops identified in well W1. A corridor stack generated from the upgoing VSP wavefield enhanced reflection visibility and facilitated comparison with reflections interpreted on the HR-1 seismic section, allowing the tops of the Comenditi, Nuraxi, and Monte Crobu volcanic formations to be confidently assigned. ERT tomography profiles revealed distinct resistivity patterns on either side of well W1. Lower resistivity values were observed to the southeast, towards the planned injection well. This trend is consistent with the geological interpretation of seismic line HR-1, as confirmed by integrating the seismic and 2D resistivity sections. The resistivity distribution supports the presence and activity of the Matzaccara Fault. The integrated geophysical investigations at the SFL site provided the essential framework for designing, positioning, and instrumenting the injection well. Although the initial feasibility study assumed a deviated well trajectory, drilling a vertical well did not compromise the modelling results.

Simulations show that the detectability of CO<sub>2</sub>-induced seismic velocity changes remains high in a vertical configuration, particularly when the injection well is incorporated into a crosswell monitoring scheme. The modelling also underscores the importance of permanent downhole instrumentation, especially fibre-optic cables for DAS measurements, to detect small velocity perturbations associated with CO<sub>2</sub> migration. The drilled injection well has encountered the fault at a depth of about 100 m, confirming the validity of the geophysical analysis. It is important to note that SFL is a test site for studying the effectiveness of monitoring techniques to detect possible leakage of CO<sub>2</sub> injected near a fault at a depth of around 300 m, and so, it does not replicate the conditions of a real industrial project where CO<sub>2</sub> is injected below 800 m. Instead, the geophysical data acquired for site characterisation not only provide information on subsurface geometries at and around the wells and allow imaging of the fault, which will be the target of future injection experiments, but they also yield insights into the petrophysical properties of the rock formations present. Seismic data provide indirect information but allow the spatial extension of these observations and form the basis for correlating well log data acquired at the borehole with the wider study area. In general, the integration of seismic and borehole geophysical measurements allows the identification of lithological contrasts, fracture zones, and fault-related damage zones that strongly influence fluid flow [40,41]. Variations in seismic attributes and electrical properties can be related to changes in porosity, permeability, and fluid saturation, supporting the assessment of injectivity and plume evolution [42,43]. Moreover, detailed imaging of fault geometry and its continuity is essential to evaluate whether faults act as sealing structures or preferential migration pathways for CO<sub>2</sub> [44–46].

## 6. Conclusions

The aim of this work was to apply high-resolution geophysical characterisation of a test site to investigate the behaviour of CO<sub>2</sub> injected at a shallow fault, aiming to develop and validate a multidisciplinary workflow (HR seismics, VSP, ERT, and modelling) dedicated to monitoring the fault response to CO<sub>2</sub> migration.

This study also demonstrates the feasibility of geophysical monitoring in a volcanic context with a weak seismic response, defines operational criteria for well design and data acquisition parameters, and provides an experimental framework to test advanced monitoring techniques in a fault-controlled CCS scenario.

The presence of faults at a storage site is a critical factor for site integrity and safety due to the potential risk of leakage. Depending on their internal structure, geometry, stress state, and diagenetic history, faults may act either as high-permeability conduits that facilitate

CO<sub>2</sub> migration or as low-permeability barriers that, in this case, promote containment through structural trapping. The sealing capacity or transmissive behavior of faults is further influenced by in situ stress conditions and pressure changes induced by CO<sub>2</sub> injection, which may lead to fault reactivation and increased permeability. Future work will focus on post-injection monitoring of the test site using a range of instruments, including borehole seismic measurements, to detect and characterize CO<sub>2</sub> behavior. Rock and reservoir parameters will be integrated to better understand CO<sub>2</sub> migration mechanisms and the geomechanical properties of the fault. This approach will allow mapping of stress and pressure variations during injection and support the definition of safe operating thresholds.

The importance of this study is its demonstration that only a fully integrated geophysical approach can meet the requirements for the characterisation and long-term monitoring of fault behaviour in relation to CO<sub>2</sub> storage, which is one of the major challenges in CCS technology.

**Author Contributions:** Conceptualisation, V.V., C.B. and D.C.; methodology, V.V. and C.B.; software, B.F., P.C., F.A., M.G. (Massimo Giorgi), C.B. and F.M.; investigation, M.G. (Massimo Giorgi), F.A., A.S., M.G. (Michela Giustiniani), E.F., D.C., F.M. and F.P.; data curation, D.C., E.B., B.F., P.C., F.A., M.G. (Massimo Giorgi), M.G. (Michela Giustiniani), C.B., F.M., A.S. and F.P.; writing—original draft preparation, V.V., C.B., D.C., E.B., E.F., M.G. (Michela Giustiniani), B.F., A.P. (Alberto Pettinau) and A.P. (Alberto Plaisant); writing—review and editing, V.V., C.B. and D.C.; visualisation, C.B., V.V., D.C., B.F., P.C., F.A., M.G. (Michela Giustiniani), A.P. (Alberto Pettinau) and A.P. (Alberto Plaisant); supervision, V.V. All authors have read and agreed to the published version of the manuscript.

**Funding:** This research was funded by the European Union’s Horizon 2020 research and innovation programme under Grant Agreement No. 653718 (Enabling Onshore CO<sub>2</sub> Storage in Europe—ENOS).

**Data Availability Statement:** The raw data supporting the conclusions of this article will be made available by the authors on request.

**Acknowledgments:** The authors acknowledge the technical staff of OGS for the acquisition of the geophysical data presented in this work.

**Conflicts of Interest:** Authors Alberto Pettinau and Alberto Plaisant are employed by the company Sotacarbo S.p.A. The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

## References

1. IEA. *World Energy Investment 2023 Report*; IEA: Paris, France, 2023. Available online: <https://www.iea.org/reports/world-energy-investment-2023> (accessed on 5 November 2025).
2. IEA. *CCUS in Clean Energy Transitions*; IEA: Paris, France, 2020. Available online: <https://www.iea.org/reports/ccus-in-clean-energy-transitions> (accessed on 20 October 2025).
3. Net-Zero Industry Act: Regulation (EU) 2024/1735 of the European Parliament and of the Council of 13 June 2024 on Establishing a Framework of Measures for Strengthening Europe’s Net-Zero Technology Manufacturing Ecosystem and Amending Regulation (EU) 2018/1724 (Text with EEA Relevance). PE/45/2024/REV/1. OJ L, 2024/1735, 28.6.2024. Available online: <http://data.europa.eu/eli/reg/2024/1735/oj> (accessed on 15 September 2025).
4. Awan, M.M.A.; Kirmani, F.U.D. Achieving low-carbon future through CO<sub>2</sub> storage. A comprehensive review of global projects and policies. *Pet. Res.* **2025**, *10*, 636–658. [[CrossRef](#)]
5. Raihan, A. Carbon capture, utilization, and storage (CCUS) in the context of earth energy systems: A multidisciplinary review. *Geosci. Front.* **2025**, *16*, 102177. [[CrossRef](#)]
6. EUR-lex. *Directive 2009/31/EC of the European Parliament and of the Council of 23 April 2009 on the geological storage of carbon dioxide and amending Council Directive 85/337/EEC, European Parliament and Council Directives 2000/60/EC, 2001/80/EC, 2004/35/EC, 2006/12/EC, 2008/1/EC and Regulation (EC) No 1013/2006*; EUR-lex: Luxembourg, 2009.

7. Stork, A.; Poletto, F.; Draganov, D.; Janssen, M.; Hassing, S.; Meneghini, F.; Böhm, G.; David, A.; Farina, B.; Schleifer, A.; et al. Monitoring CO<sub>2</sub> injection with passive and active seismic surveys: Case study from the Hellisheiði geothermal field, Iceland. In Proceedings of the 16th Greenhouse Gas Control Technologies Conference (GHGT-16), Lyon, France, 23–27 October 2022. [[CrossRef](#)]
8. Fais, S.; Ligas, P.; Cuccuru, F.; Maggio, E.; Plaisant, A.; Pettinau, A.; Casula, G.; Bianchi, M.G. Detailed petrophysical and geophysical characterization of core samples from the potential caprock-reservoir system in the Sulcis Coal Basin (Southwestern Sardinia–Italy). *Energy Procedia* **2015**, *76*, 503–511. [[CrossRef](#)]
9. Tartarello, M.C.; Plaisant, A.; Bigi, S.; Beaubien, S.E.; Graziani, S.; Lombardi, S.; Ruggiero, L.; De Angelis, D.; Sacco, P.; Maggio, E. Preliminary results of geological characterization and geochemical monitoring of Sulcis Basin (Sardinia), as a potential CCS site. *Energy Procedia* **2017**, *125*, 549–555. [[CrossRef](#)]
10. Buttinelli, M.; Procesi, M.; Cantucci, B.; Quattrocchi, F.; Boschi, E. The geo-database of caprock quality and deep saline aquifers distribution for geological storage of CO<sub>2</sub> in Italy. *Energy* **2011**, *36*, 2968–2983. [[CrossRef](#)]
11. Civile, D.; Zecchin, M.; Forlin, E.; Donda, F.; Volpi, V.; Merson, B.; Persoglia, S. CO<sub>2</sub> geological storage in the Italian carbonate successions. *Int. J. Greenh. Gas Control* **2013**, *19*, 101–116. [[CrossRef](#)]
12. Donda, F.; Civile, D.; Forlin, E.; Volpi, V.; Zecchin, M.; Gordini, E.; Merson, M.; De Santis, L. The northernmost Adriatic Sea: A potential location for CO<sub>2</sub> geological storage? *Mar. Pet. Geol.* **2013**, *42*, 148–159. [[CrossRef](#)]
13. Volpi, V.; Forlin, E.; Baroni, A.; Estublier, A.; Donda, F.; Civile, D.; Caffau, M.; Kuczynsky, S.; Vincké, O.; Delprat-Jannaud, F. Evaluation and characterization of a potential CO<sub>2</sub> storage site in the south Adriatic offshore. *Oil Gas Sci. Technol.* **2015**, *70*, 695–712. [[CrossRef](#)]
14. Carmignani, L.; Pertusati, P.C.; Barca, S.; Carosi, R.; Di Pisa, A.; Gattiglio, M.; Musumeci, G.; Oggiano, G. *Struttura della Catena Ercinica in Sardegna. Guida All’Escursione*; Centrooffset Siena: Siena, Italy, 1992; pp. 1–177.
15. Costamagna, L.; Barca, S. The Germanic Triassic of Sardinia (Italy): A stratigraphic, depositional and palaeogeographic review. *Riv. Ital. Paleont. Strat.* **2022**, *108*, 67–100. [[CrossRef](#)]
16. Costamagna, L.G.; Schäfer, A. Evolution of a Pyrenean molassic basin in the Western Mediterranean area: The Eocene–Oligocene Cixerri Formation in Southern Sardinia (Italy). *Geol. J.* **2018**, *53*, 424–437. [[CrossRef](#)]
17. Fanni, S.; Murru, M.; Salvadori, A.; Sarria, E. Nuovi dati strutturali sul Bacino Del Sulcis. *L’Ind. Mineraria* **1982**, *4*, 25–31.
18. Murru, M.; Salvadori, A. Ricerche stratigrafiche sul bacino del Sulcis (Sardegna sudoccidentale). I depositi continentali paleocenici della Sardegna meridionale ed il loro significato paleoclimatico. *Geol. Rom.* **1987**, *26*, 149–165.
19. Ottelli, L.; Perna, G. *Carta Geologica del Bacino Carbonifero del Sulcis (Sardegna Sud Occidentale)*; S.E.L.C.A.: Florence, Italy, 1993.
20. Deiana, G.; Carmignani, L.; Orrù, P.; Sale, V.; Pintus, C.; Pisanu, G.; Ulzega, A.; Pasci, S. *Note Illustrative della Carta Geologica d’Italia alla Scala 1:50.000, F. 564 Carbonia*; Servizio Geologico d’Italia—ISPRA: Rome, Italy, 2012. [[CrossRef](#)]
21. Bigi, S.; Tartarello, M.C.; Ruggiero, L.; Graziani, S.; Beaubien, S.; Lombardi, S. On-going and future research at the Sulcis site in Sardinia, Italy—Characterization and experimentation at a possible future CCS pilot. *Energy Procedia* **2017**, *114*, 2742–2747. [[CrossRef](#)]
22. Murru, M.; Ferrara, F.; Da Pelo, S.; Ibba, A. The Paleocene–Middle Eocene deposits of Sardinia (Italy) and their paleoclimatic significance. *Comptes Rendus Geosci.* **2003**, *335*, 227–238. [[CrossRef](#)]
23. Barca, S.; Maxia, C.; Palmerini, V. Sintesi sulle attuali conoscenze relative alla “Formazione del Cixerri” (Sardegna sud-occidentale). *Boll. Serv. Geol. It.* **1973**, *94*, 307–318.
24. Barca, S.; Palmerini, V. Contributo alla conoscenza degli ambienti di sedimentazione relativi alla “Formazione del Cixerri” (Sardegna sud-occidentale). *Boll. Soc. Sarda Sci. Nat.* **1973**, *7*, 13–47.
25. Barca, S.; Costamagna, L.G. New stratigraphic and sedimentological investigations on the Middle Eocene–Early Miocene continental successions in southwestern Sardinia (Italy): Paleogeographic and geodynamic implications. *Comptes Rendus Geosci.* **2010**, *342*, 116–125. [[CrossRef](#)]
26. Assorgi, A.; Fadda, A.; Gimeno, D.; Morra, V.; Ottelli, L.; Secchi, F.A. Le successioni ignimbritiche terziarie del Sulcis (Sardegna sud-occidentale). *Mem. Della Soc. Ital.* **1990**, *45*, 951–963.
27. Assorgi, A.; Cincotti, F.; Fadda, A.; Gimeno, D.; Morra, V.; Ottelli, L.; Secchi, F.A. Il complesso comenditico miocenico dell’entroterra sulcitano (Sardegna sud-occidentale). Caratteri geologici, vulcanologici e petrochimici. *Mem. Descr. Carta Geol. D’Italia* **1994**, *49*, 347–362.
28. Morra, V.; Secchi, F.A.; Assorgi, A. Petrogenetic significance of peralkaline rocks from Cenozoic calcalkaline volcanism from SW Sardinia, Italy. *Chem. Geol.* **1994**, *118*, 109–142. [[CrossRef](#)]
29. Servizio Geologico d’Italia—ISPRA. *Carta Geologica d’Italia alla Scala 1:50.000, Foglio 564 Carbonia*; Servizio Geologico d’Italia—ISPRA: Rome, Italy, 2012. [[CrossRef](#)]
30. Plaisant, A.; Maiu, A.; Maggio, E.; Pettinau, A. Pilot-scale CO<sub>2</sub> sequestration test site in the Sulcis Basin (SW Sardinia): Preliminary site characterization and research program. *Energy Procedia* **2017**, *114*, 4508–4517. [[CrossRef](#)]

31. Anselmi, M.; Saccorotti, G.; Piccinini, D.; Giunchi, C.; Paratore, M.; De Goria, P.; Buttinelli, M.; Maggio, E.; Plaisant, A.; Chiarabba, C. Microseismic assessment and fault characterization at the Sulcis (South-Western Sardinia) field laboratory. *Int. J. Greenh. Gas Control* **2020**, *95*, 102974. [[CrossRef](#)]
32. Tedde, F.; Maiu, A.; Plaisant, A.; Pettinau, A. Experimental comparison between dynamic and static parameters for volcanic rocks in Sulcis basin (Italy). *J. Appl. Geophys.* **2023**, *217*, 105181. [[CrossRef](#)]
33. Berryman, J.G. Origin of Gassmann's equations. *Geophysics* **1999**, *64*, 1627–1629. [[CrossRef](#)]
34. Farina, B.; Parisio, F.; Poletto, F. A seismic-properties and wave-propagation analysis for the long-term monitoring of supercritical geothermal systems. *Geothermics* **2022**, *104*, 102451. [[CrossRef](#)]
35. Bell, I.H.; Wronski, J.; Quoilin, S.; Lemort, V. Pure and pseudo-pure fluid thermophysical property evaluation and the open-source thermophysical property library CoolProp. *Ind. Eng. Chem. Res.* **2014**, *53*, 2498–2508. [[CrossRef](#)] [[PubMed](#)]
36. Meneghini, F.; Poletto, F.; Bellezza, C.; Farina, B.; Draganov, D.; Van Otten, G.; Stork, A.L.; Böhm, G.; Schleifer, A.; Janssen, M.; et al. Feasibility Study and Results from a Baseline Multi-Tool Active Seismic Acquisition for CO<sub>2</sub> Monitoring at the Hellisheiði Geothermal Field. *Sustainability* **2024**, *16*, 7640. [[CrossRef](#)]
37. Bellezza, C.; Barison, E.; Farina, B.; Poletto, F.; Meneghini, F.; Böhm, G.; Draganov, D.; Janssen, M.T.G.; van Otten, G.; Stork, A.L.; et al. Multi-Sensor Seismic Processing Approach Using Geophones and HWC DAS in the Monitoring of CO<sub>2</sub> Storage at the Hellisheiði Geothermal Field in Iceland. *Sustainability* **2024**, *16*, 877. [[CrossRef](#)]
38. Fais, S.; Ligas, P.; Cuccuru, F.; Pala, A. Caratterizzazione di una zona di faglia nell'area del bacino del Sulcis: Profili elettromagnetici. In *Rapporto Tecnico ENEA; Report RdS/PAR2015/248; Agenzia Nazionale per le Nuove Tecnologie, l'Energia e lo Sviluppo Economico Sostenibile (ENEA): Roma, Italy, 2016.*
39. Pánek, T.; Margielewski, W.; Táborík, P.; Urban, J.; Hradecký, J.; Szura, C. Gravitationally induced caves and other discontinuities detected by 2D electrical resistivity tomography: Case studies from the Polish Flysch Carpathians. *Geomorphology* **2010**, *123*, 165–180. [[CrossRef](#)]
40. Rutqvist, J. The geomechanics of CO<sub>2</sub> storage in deep sedimentary formations. *Geotech. Geol. Eng.* **2012**, *30*, 525–551. [[CrossRef](#)]
41. Faulkner, D.R.; Jackson, C.A.-L.; Lunn, R.J.; Schlische, R.W.; Shipton, Z.K.; Wibberley, C.A.J.; Withjack, M.O. A review of recent developments concerning the structure, mechanics and fluid flow properties of fault zones. *J. Struct. Geol.* **2010**, *32*, 1557–1575. [[CrossRef](#)]
42. Ayani, M.; Grana, D. Statistical rock physics inversion of elastic and electrical properties for CO<sub>2</sub> sequestration studies. *Geophys. J. Int.* **2025**, *223*, 707–724. [[CrossRef](#)]
43. Chadwick, A.; Clochard, V.; Delepine, N.; Labat, K.; Sturton, S.; Buddensiek, M.-L.; Dillen, M.; Nickel, M.; Lima, A.L.; Arts, R.; et al. Quantitative analysis of time-lapse seismic monitoring data at the Sleipner CO<sub>2</sub> storage operation. *Lead. Edge* **2010**, *29*, 170–177. [[CrossRef](#)]
44. Caine, J.S.; Evans, J.P.; Forster, C.B. Fault zone architecture and permeability structure. *Geology* **1996**, *24*, 1025–1028. [[CrossRef](#)]
45. Chen, Z.; Cui, G.; Liu, Z.; Zhao, L.; Niu, Z.; Feng, X.; Hu, Z.; Zhang, Q.; Tian, H.; Ning, F. Fault stability and sealing capacity evolution during CO<sub>2</sub> geological sequestration on different injection strategies. *Energy* **2025**, *332*, 137170. [[CrossRef](#)]
46. Zappone, A.; Rinaldi, A.P.; Grab, M.; Wenning, Q.C.; Roques, C.; Madonna, C.; Obermann, A.C.; Bernasconi, S.M.; Brennwald, M.S.; Kipfer, R.; et al. Fault sealing and caprock integrity for CO<sub>2</sub> storage: An in situ injection experiment. *Solid Earth* **2021**, *12*, 319–343. [[CrossRef](#)]

**Disclaimer/Publisher's Note:** The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content.